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3D Modeling of the Thermal Coagulation Necrosis Induced by an Interstitial Ultrasonic Transducer

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Abstract

This paper describes a temperature-varying attenuation approach for pre-operative planning of high intensity ultrasound interstitial targeted therapy. Such approach is mainly aimed at the treatment of primary liver cancer for which a precise lesion control must be achieved. It is shown through simulation that the shape and size of the resulting necrotic volume is significantly different from the one obtained when this tissue property is considered constant in time.

Index terms

High intensity ultrasound therapy, hyperthermia, interstitial therapy, planning, simulation, tissue properties.

1 Introduction

Hepatocellular carcinoma or primary liver cancers lead to more than 1 million new cases diagnosed each year. Although less common in the western countries, its incidence is rising [1]. At early stages, hepatocellular carcinoma is confined to a solitary mass and is therefore potentially curable by surgical resection [2]. However, tumors can be localized but unresectable due to critical anatomical environment, concomitant disease such as cirrhosis or even bilateral locations. These patients may then undergo percutaneous surgery (percutaneous ethanol injection, or radiofrequency) [3]. An alternative based on high intensity ultrasound therapy is proposed using a similar interstitial approach [4]. Interstitial ultrasound offers the advantage to be more controllable in depth and direction than other interstitial heating modalities. Like any other minimally invasive image guided therapy, its clinical application requires an efficient planning at the pre-operative stage, and an accurate tracking and control during the intra-operative phase. Thus, in addition to the classical image processing issues (segmentation, registration,

rendering, etc.), a sound physically-based model of the thermal dose to be delivered must be designed that should be updated according to the temperature measurements when the intervention is performed. A first computer simulation tool for high energy ultrasound therapy has been reported in [5] which relied on tissue spatial homogeneity and invariance of its acoustic properties. However, this tool proposed an exact pressure field estimation. More recently, Mast et al [6] proposed an enhanced model, but with a planar transducer geometry limitation and mathematical simplifications, which have an influence on the pressure field computation especially close to the simulated transducer. To go further, we propose a model which relies on a balance between complexity and computation time. In this paper, we introduce time-varying properties of the tissue during ultrasound application together with accelerated techniques for dose computation. Section 2 provides the basic features of the model and Section 3, an example illustrating the difference in the necrotic size estimation that can be observed between invariant and variable tissue properties hypotheses.

2 Method

2.1 Transducer geometry and control

The modeled therapeutic ultrasound device (Fig. 1) was composed of a small (3 mm x 10 mm) planar ultrasonic mono-element transducer encapsulated in a cylindrical interstitial applicator. The transducer operated at a single frequency between a range from 5 to 15 MHz depending on its geometrical design. The transducer was air-backed, so ultrasound was only propagated forward. The front transducer face was cooled by a continuous flow of degassed water maintained at a constant temperature (5 °C in the therapeutic case) . The therapy consisted in a sequence of exposures. After each exposure the applicator was rotated by a specific angle in order to deposit heat according to the tumor geometry. The planning parameters are the exposure duration; the ultrasonic intensity (measured by a force balance at the surface of the applicator); the angular step between two adjacent elementary exposures and the total angle of treatment.

2.2 Computer simulation

The modeling can be summarized as follows:

1. Each shot produces a pressure field p . The calculated pressure field depends on the physical and the tissue assumptions. This point will be addressed in section 2.3.
2. The energy of the beam is converted into heat. The tissue temperature evolution over time is obtained by solving Pennes' bioheat transfer equation (BHTE) [7] which describes thermal processes in human perfused tissues. The BHTE has the following 3D+t form:

$$\rho_t C_t \frac{\partial T}{\partial t} = k_t \nabla^2 T + V \rho_b C_b (T_a - T) + Q \quad (1)$$

where T is the temperature and ρ_t , C_t , k_t , V , ρ_b , and C_b are respectively the density, the specific heat and thermal conductivity of tissues, the perfusion rate per unit volume of tissues, the density and the specific heat of blood. This equation describes the variation of energy per unit of volume. In (1), it can be seen that this variation can be divided into three terms (from left to right): the thermal diffusion, the effect of perfusion and Q the acoustic power provided by the exposures. Q is directly deduced from the simulated pressure field ($Q \propto p^2$). A finite difference method was used to solve this equation [8]. The temperature of the cooling water serves as an iso-thermal boundary condition. As ebullition was not considered in the present model and for avoiding unrealistic temperatures; a threshold ensures that the temperature could never exceed 100 °C. We take also the tissue necrosis into account: the perfusion rate V is set to zero when tissues are necrosed.

3. The concept of thermal dose [9], which is quite standard in tumor hyperthermia literature, was used to assess thermal damages. For each location and history of temperature, the thermal dose is defined as an equivalent time the temperature of reference of 43 °C should be applied to obtain the same thermal damage. It can be computed directly from the temperature map:

$$D_{43^{\circ}\text{C}}(x, y, z, t) = \sum_{i=1}^t R^{(43-T(x,y,z,t))} \Delta t \quad (2)$$

with $R = 0.5$ if $T > 43^{\circ}\text{C}$ and $R = 0.25$ otherwise.

4. Liver tissues are considered as irreversibly thermally damaged when $D_{43^{\circ}\text{C}} > 340$ minutes [10].

2.3 Calculation of the pressure field

The determination of the pressure field is one major feature of the overall process. Numerical methods for estimating the pressure field can take into account the nonlinear propagation of high intensity waves [11, 12, 13] or remain purely linear. In our study, with a non-focused plane transducer, the propagation can be considered linear [14]. From this assumption, the pressure field can be exactly computed for the entire volume on the basis of the Rayleigh integral with O'Neil's hypotheses [5]. The goal is thus to compute the acoustic pressure at a location point M ; the transducer of surface S is sampled into elements of surface ΔS which size is negligible in comparison with the wavelength λ ; M and one element of surface ΔS are connected by a straight segment ΔSM of length l sampled into elements Δl . The pressure at a location M is given by the discrete version of the Rayleigh integral:

$$p(M) = \left| \sum_S j \frac{p_0}{\lambda} \Delta S \frac{\exp^{-jkl}}{l} \exp^{-f \sum_{i=1}^l \alpha_i \Delta l} \right| \quad (3)$$

with p_0 the pressure at the transducer surface (Pa), k the wave number ($2\pi/\lambda$), f the transducer frequency (Hz) and α_i the tissue attenuation coefficient at location i along the line segment ΔSM ($\text{Np} \cdot \text{cm}^{-1} \cdot \text{MHz}^{-1}$).

This twofold integration (over the surface of the transducer and the segment ΔSM) is very computation intensive. Some simplifications are usually made in order to accelerate the simulation [5]: the tissues are assumed to be homogeneous around the applicator and its physical properties (the tissue attenuation coefficient) constant in time. They have the three following benefits:

- The propagation of a wave from one element of surface ΔS to M is carried through only 2 media: the cooling water of the transducer (α_1, l_1) and the tissues (α_2, l_2). Because α_1 is negligible and p_0 is estimated at the surface of the applicator, the equation (3) can therefore be simplified as:

$$p(M) = \left| \sum_S j \frac{p_0}{\lambda} \Delta S \frac{\exp^{-jkl}}{l} \exp^{-f \alpha_2 l_2} \right| \quad (4)$$

- The simulated air-backed transducer providing only forward waves and the homogeneous medium of propagation allow computing pressure in a quarter of a space in front of the propagation axis only for symmetry reasons.

- Regardless to the applicator orientation, the generated pressure field remains constant in the transducer coordinates system. So, the pressure field generated after the rotation of the applicator can simply be obtained by an angular shift of the first estimated pressure field matrix. The necrosis simulation can be summarized as : 1) estimation of the pressure field for one exposure; 2) temporal integration of this pressure field within the BHTE (1) after rotation by the planned angles.

Adaptative sampling of the transducer and volume of calculation allows a relatively fast pressure field computation time (8 minutes on a conventional PC: AMD Athlon 2200+ proc. with 1MB RAM).

2.4 Dynamic tissue attenuation coefficient variation

The attenuation coefficient associated to a given tissue is no more constant over time. This coefficient changes as temperature changes and as tissue necroses. The attenuation coefficient curves (ie coefficient variation vs. temperature) was measured for various tissues [15]. For liver, Connor et al. [13] made a 6th order polynomial approximation of the experimental data (see curve in Fig. 2).

Taking this attenuation coefficient variation into account modifies the simulation framework described in section 2.2: 1) the pressure field is first computed and then incorporated into the BHTE; 2) according to the computed temperatures, the tissue attenuation coefficients at each location of the volume are updated; 3) a new pressure field is then estimated and so on.

The consequence of this time-varying behavior is that the hypothesis of homogeneity and time invariance of the tissue properties is no more true. The three previous described simplifications (analytical integration simplification of (4), symmetry and pressure field invariance) cannot be used anymore. The brute force algorithm based on (3) induces a tremendous computing time for the overall necrosis estimation. However, several simplifications can be proposed in order to reasonably reduce this computing time without losing accuracy on the estimate of the necrosed volume:

- Within the BHTE, the temperature variation is relatively slow, so the tissue attenuation coefficient variation is slow too. Two different time steps can be considered: a fast one ($\Delta t = 0.02s$) for resolving the BHTE (1) and a longer one (2s) for updating the attenuation coefficients and the pressure field.
- The tissue attenuation coefficient curves is stepwise approximated (Fig 2). This allows to cluster the volume elements into larger regions with constant tissue coefficients. The segment ΔSM crosses now regions with a constant attenuation coefficient α_i over a distance l_i . Equation 3 can then be rewritten as:

$$p(M) = \left| \sum_S j \frac{p_0}{\lambda} \Delta S \frac{\exp^{-jkl}}{l} \exp^{-f \sum_{i=1}^N \alpha_i l_i} \right| \quad (5)$$

Where N denotes the number of crossed regions along the segment ΔSM .

- Segment coherence was also considered: adjacent ΔSM segments share almost the same attenuation properties. For nine adjacent connected transducer surface element ΔS , we compute the $\exp^{-f \sum_{i=1}^N \alpha_i l_i}$ term of equation 5 for only the ΔSM segment which originates from the central surface element and apply this term to the segments which originate from the eight adjacent surface elements.

These simplifications, with the volume and transducer adaptive sampling mentioned in section 2.3, allow reducing the computation time to around 16h30. Some optimizations are still under study in order to keep diminishing the computation time.

2.5 Experimental validation of the model

For comparison, an experiment was performed *in vivo* [4]. The transducer was positioned inside the liver of a pig, away from large blood vessels. This animal experimentation was approved by a veterinarian ethics committee. At the time of the study we only had at our disposal a 10.7 MHz transducer. The exposure conditions were set to: 14 W/cm² for the intensity measured by a force balance at the surface of the applicator; 37 °C for the transducer cooling water temperature and 20 s for the duration of the exposure. Four thermocouples were introduced inside liver on the acoustic axis of the transducer right at the end of the 20 s-long exposure. The maximum increase of temperature was measured at four different positions: 2.5, 5, 7.5 and 10 mm from the applicator surface.

3 Results and Discussion

Our goal is to simulate a real therapy. In order to maximize the necrotic volume size, we choose to develop a 5 MHz therapeutic ultrasound device with an intensity of 40 W/cm² measured by a force balance at the surface of the applicator and a constant cooling water temperature of 5 °C. The simulated therapy strategy consisted of a sequence of twenty six 3 s-long exposures. The transducer was rotated by 3.6 ° after each exposure. Thus, the device swept a 90 ° angle. The tissues, perfusion and blood parameters were found in the literature [16, 17, 18].

Fig. 3 shows the maximum temperature field obtained during the sequence (3-a and 3-b) and the obtained necrotic volume final form (3-c and 3-d) in an axial XY cut plan at $z = 0$ (see the coordinates system on Fig. 1). Figures 3-a and 3-c were obtained considering homogeneous tissues (4) while figures 3-b and 3-d included the variation of attenuation coefficients with temperature (5).

The simulations point out that the obtained maximal temperatures increased higher and faster near the transducer when the attenuation varied with temperature. The attenuation coefficient increased principally over a limited depth, close to the transducer, where heating is more intense. Most of the acoustic power is then absorbed near the transducer with the effect to decrease the available power deposit at more distant regions. The consequence is that the proximal heating is enhanced even more and the distal heating is decreased. Furthermore the size of the necrotic volume is naturally reduced in the direction of propagation. This can be observed on Fig. 3: the temperature field, the thermal dose field and so the necrotic volume were less extended in the radial direction. This observation is particularly true at the end of the movement of the transducer ($\Theta = 90^\circ$). In the radial distance from the transducer, the necrotic volume reaches a distance of 15 mm when attenuation coefficient is constant, but only 11 mm when the necrotic volume is estimated using the temperature dependent attenuation coefficient. Some changes can also be noticed along the Z axis where the temperature field and so the necrotic volume are less extended of about 2 mm on that direction when coefficients vary with temperature. The dissymmetrical shape of the necrosis is due to the fact that the increase of temperature in tissues is still low for the first elementary exposures, while successive exposures benefit from previous exposures. Consequently, the decrease in the necrotic volume size, for higher rotation angle of treatment, is more substantial because of higher attenuation coefficients.

These facts are confirmed by the experimental validation of the model presented on section 2.5. Fig. 4 compares the real temperatures measured on the *in vivo* experimental validation at the four different positions and the temperature curves obtained by the two simulation methods initialized by the parameters of the experimental protocol described in [4]. The temperature curve obtained by the approach using attenuation coefficient variation with temperature is closer to the experimental data.

This approach, that takes into account the variation of attenuation with temperature, shows

significant changes in both the size and the shape of the necrotic volume. Therefore and in spite of the computing time, it is important to integrate this phenomenon and other complex tissue properties into the model (vascular structures proximity, vaporization...). Defining and optimizing the planning parameters with accuracy would permit to obtain a more precise adapted therapy. The next step would be to run more experiments that are relevant to the treatment strategy (juxtaposition of elementary exposures) in order to validate the model. The comparison could be based on the *in vivo* macroscopic evaluation of the thermal lesion or on temperature maps recorded during treatment by MRI [19, 20].

4 Conclusion

A method simulating the formation of necrosis generated by high intensity ultrasound was described. The classical model assumed that tissues are homogeneous with physical properties invariant during the treatment. Instead of that assumption, we introduced a new model which takes into account the variation of the tissue attenuation coefficient. This method predicts the size and shape of the necrotic volume with a better accuracy and so allows a more precise therapy planning.

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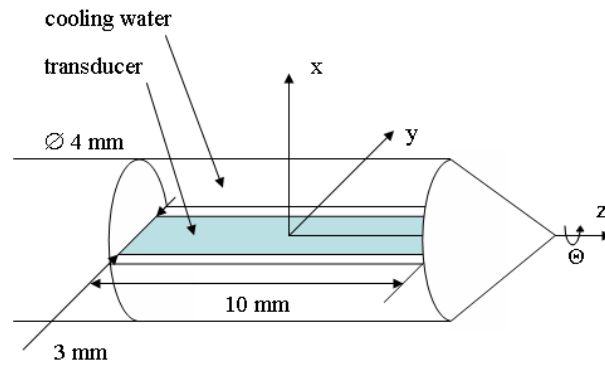


Figure 1: Transducer geometry.

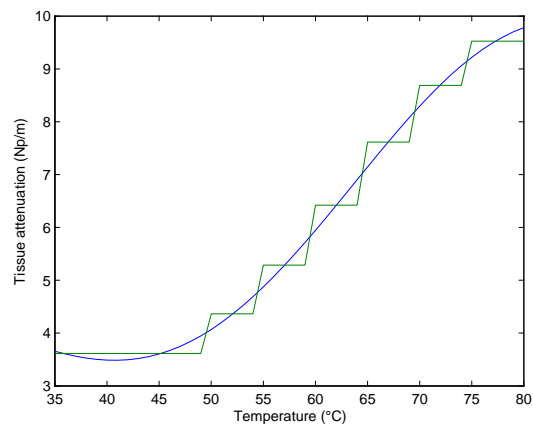


Figure 2: Continuous and stepwise linearized tissue attenuation coefficient vs. temperature.

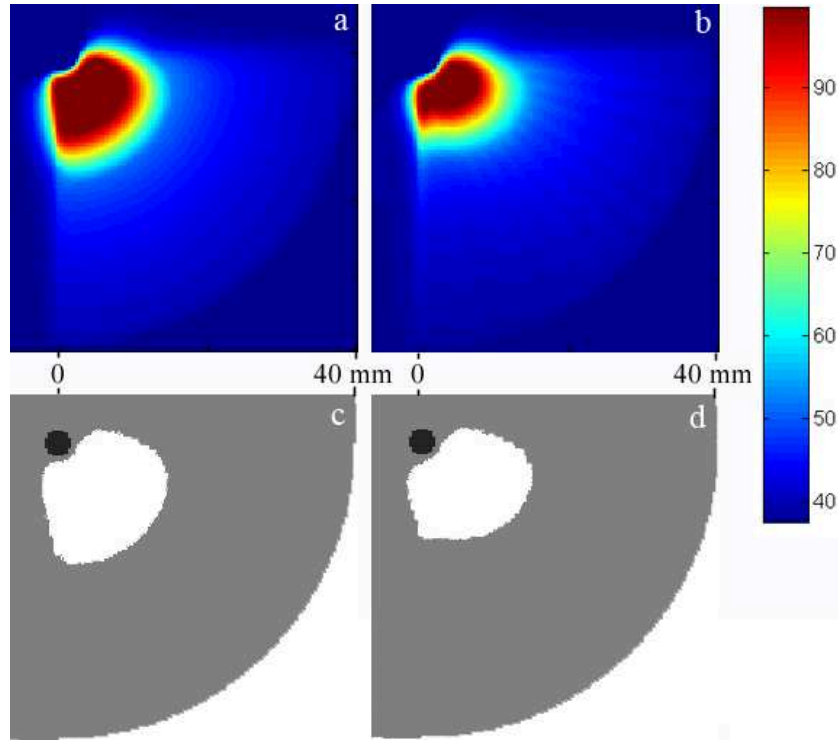


Figure 3: Temperature pattern and necrotic volume obtained with the tissue homogeneity hypotheses (a and c) and attenuation coefficient variation with temperature (b and d). Temperature scale in $^{\circ}\text{C}$.

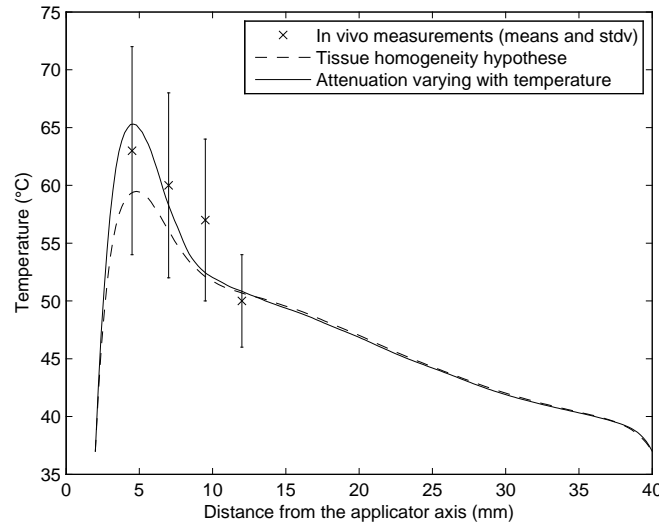


Figure 4: Comparison between the experimental *in vivo* temperature measurements and the simulated temperatures obtained with the tissue homogeneity hypotheses and attenuation coefficient variation with temperature.